

AVIATION AND AERONAUTICAL ENGINEERING



Photos by Central News Photo Service

King George and Queen Mary Visit an Aerodrome

OCTOBER

15th

1916

SPECIAL FEATURES

ORGANIZATION OF ARMY AVIATION SECTION
DEVELOPMENT OF THE ZEPPELIN AIRSHIP
THE CURTISS 250 HORSEPOWER MOTOR
OUTLINED COURSE FOR THE TRAINING OF AVIATORS
THE NATIONAL ADVISORY COMMITTEE MEETING
THE COURSE IN AERODYNAMICS AND AEROPLANE DESIGN

PRICE

Ten

Cents

PUBLISHED SEMI-MONTHLY
BY
THE GARDNER, MOFFAT CO., Inc.
120 W. 52nd ST. NEW YORK



THE STURDINESS of the Sturtevant Aeronautical Motor is clearly proven by this unretouched photograph.

This was a time exposure made while motor was running at 2000 R.P.M.

This vibrationless operation means sturdiness of design, accuracy of construction, long life, and high efficiency.

Sturtevant

MADE IN U.S.A. PAT. APP'D

B. F. STURTEVANT COMPANY

Hyde Park, Boston, Massachusetts.



OFFICIAL Government aircraft of Marine Trucks and Seaplanes give them their enviable position in the aviation world.

RECONNAISSANCE Type R is designed especially for greatest efficiency. Span 46' 5". Length 27'. Area supporting surface 400 sq. ft. Two-wheel landing gear. Weight empty 1740 pounds. Useful load 760 pounds. With this load we guarantee speed range 45 to 86 miles per hour; glide 8-1, climb 3000' in 10 minutes.

DELIVERIES January First. Present output sold until then. Price \$10,500.

Glenn L. Martin Company
Los Angeles, Cal.



BURGESS FLYING BOAT



After conclusive tests the Burgess Company offers a water and air craft ideal for sport-cruising.

Safety and comfort never before attained in flying is rendered in this latest model boat under the patents of Burgess, Curran and Dunner.

The crew is seated in a steady, roomy hull, provided with wind and spray shields, deep cushions, lockers, and all the appointments of a modern high-speed launch.

Absolute inherent balance is assured by the Dunner system, a balance as certain and simple as that afforded by the keel of a sailing yacht.

Steering is effected in a single wheel with duplicate control for pilot and passenger.

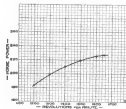
The engine may be started without leaving the cockpit.

The construction is worked out with a motto of detail which means the sure to be appreciated.

THE BURGESS COMPANY, Marblehead, Mass.

NOTICE

Owing to changes and improvements our 5" x 7" eight-cylinder motor, formerly known as Model "VX" rated at 160 horsepower, will hereafter be known as Model "VX-3" and will be rated at 200 horsepower. The following is a record of electric dynamometer test of stock motor "VX-3" No. 3512 as delivered from the Production Department.



CURTIS AEROPLANE & MOTOR CORPORATION

Buffalo, N. Y.

Duration of test (minutes)	60
Average E. P. M.	1495.31
Average load on scales (lbs.)	445.54
Average horsepower	208.21
Maximum observed horsepower	220.20
Minimum observed horsepower	198.40
Total Gas consumption (lbs.)	0.21.29
Total Gas consumption (U. S. gals.)	0.34.91
Gas consumption per hour (lbs.)	0.31.29
Gas consumption per hour (U. S. gals.)	0.50.15
Gas consumption (lbs. per H. P. hour)	0.0015
Total Oil consumption (lbs.)	6.30
Total oil consumption (U. S. gals.)	0.84
Oil consumption (U. S. gals. per hour)	0.014
Oil pressure—out of test (lbs.)	11.00
Oil pressure—out of test (lbs.)	11.00
Oil pressure—maximum test (lbs.)	24.00
Oil pressure—minimum test (lbs.)	08.00
Average water Temp. (F.)	105.00
Average inlet water Temp. (F.)	107.00

HALL-SCOTT



Exhaust Side
90-100 H. P.

Upon Sept. 16, 1916, Mr. Graham, detailed from the United States Army headquarters, Washington, D. C., to the HALL-SCOTT factory, conducted a five hour non-stop test with a HALL-SCOTT 90-100 H. P. 4-cylinder aviation motor. The results obtained were as follows:

Average revolutions per minute	1340
" brake H. P. developed	199.5
" gasoline consumption per hour	8.55
" oil consumption per hour	1.5 Gal.

A MOTOR WITH SUCH STURDINESS, DEPENDABILITY, AND SIMPLICITY OF DESIGN AS THE HALL-SCOTT 90-100 4 CYLINDER, IS DESTINED TO TAKE A LEADING PART IN THE EQUIPMENT FOR ARMY AND NAVY SCHOOLING AND LIGHT SCOUTING AIRPLANES.

HALL-SCOTT MOTOR CAR CO., Inc.

General offices:---818 Crocker Bldg., San Francisco, Calif.

Eastern representative: F. P. Whitaker, 165 Broadway, N. Y.



Wright Flying School Graduates

are universally accepted as skilled and accomplished aviators. Many of these flying men whose names are emblazoned in the annals of flight were Wright students.

Our instructors have flown Wright machines for many years and have specialized in training work.

The School is located on the Hempstead plains, one of the great world flying fields—665 acres of treeless land and a hundred square miles over which to safely fly. It is convenient to New York, with steam and electric trains and fast automobile routes.

Camping facilities on the field for the out-of-door man. Good living accommodations within easy reach.

All instruction is in the air. Dual controls. The Student is taken into the air on the first lesson.

Send for Booklet

WRIGHT FLYING FIELD, Inc.
60 Broadway, New York



OCTOBER 15, 1916

AVIATION AND AERONAUTICAL ENGINEERING

VOL. 1. NO. 6

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THE CREAGH-OSBORNE AIR COMPASS

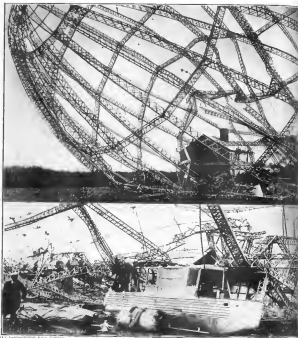
Built especially for air service, The Creagh-Osborne Compass incorporates the following advantages:

- 1.—Its radium-figured dial can be accurately read by its own light independent of any other illumination.
- 2.—The prismatic reflector, by its magnifying effect, allows the use of a small dial with the ease of reading of a large card.
- 3.—The instrument is so designed as to have a large angle of heel.
- 4.—It is of wonderfully light, compact construction.



A product of "Sperry Quality" throughout. May we tell you more about it?

THE SPERRY GYROSCOPE COMPANY
Manhattan Bridge Plaza
BROOKLYN, N. Y.
18 Victoria Street
LONDON, E. C.
8 Rue Daumesnil
PARIS



(U. S. International Film Corp.)

Two views of a Zeppelin structure shown here in detail and. The structure is shown in detail, and the various struts and beams are clearly visible. The lower view shows one of the struts.

PLANNING AND DESIGN
LESTER D. GARDNER

DESIGN AND CONSTRUCTION
PHILIP J. ROBERTS

AVIATION AND AERONAUTICAL ENGINEERING

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Vol. 1

October 21, 1935

No. 4

TWO announcements made by the Aviation Section of the Signal Corps of the Army in the last few days will go far toward convincing the public that solid progress is being made to create a substantial aviation service. Right present some machines have been ordered, four of the Curtiss triplane type and four Stearman biplanes. These speedy mounts are, if installed as units are true, practically equal to foreign aircraft of the best military present types.

These new units of war were clearly explained in the memorandum issued by the War Department, and published exclusively in AVIATION, and AVIATION, and AVIATION, on September 15. By ordering these new types almost immediately after the initial body, the Aviation Section has shown that it is prepared to undertake the construction of a type of aircraft to preserve, to promote development of the type, it is convinced will be superior for active military duty. Another significant fact about this order is that a triplane has been accepted. As will be seen from the picture elsewhere in this issue, it is a radical development in airplane design and its acceptance by the War Department gives splendid proof of a willingness to accept aeronautical engineers in developing new ideas in construction.

In this issue will be found the tentative plans for the permanent organization of the Aviation Section, the requirements for service in the Officers Reserve Corps, the requirements for the Enlisted Reserve Corps, the regulations for Civilian Aviation Schools and the method to be followed for application in National Guard units.

The great importance of this announcement will be evident to all who have been informed by the outstanding reports that have been widely circulated. It will settle all questions regarding the qualifications, service, remuneration and pressure in the permanent of an aviation service. It is to be hoped that many of the aviators whose names were published in our last issue will report as requested for admission. It would be an opportunity to the country if some of the American flyers who possess an internationally famous could offer their services for the reserve corps.

To those who have been led to believe that every aviator could become an officer in the simple equivalent of taking a few months training at an army aviation school the plans will be disappointing. An officer in the United States Army has always represented himself as well as fighting ability. The officers of the Army Reserve Corps will be required to come up to the standard set for all other reserve officers. For this reason the requirements call for "the equivalent of a college education."

There should be no misunderstanding of this phrase. It is a qualification that is used to apply to all reserve officers. It is a need as a qualification for admission to any of the corps such as the Plattburg training camp and simply means that to be accepted a man must have at least as much experience of the world as is demanded by a college education. No one ought to be deterred from making application for the Officers Reserve Corps because he has not been to college.

By the ordering of the present machines and announcing the tentative Reserve plans the Aviation Section has taken a great first step toward solving both the material and personnel problems. The public, disturbed by unimpressive reports, will find in these progressive steps cause for genuine confidence in the ability and efficiency of the Aviation Section.

Suggestions for Aeronautical Motors

THIS ISSUE OF AVIATION AND AERONAUTICAL ENGINEERING contains some quotations from the minutes of the public meeting of the Executive Committee of the National Advisory Committee for Aeronautics. This meeting was called in order to signify the new order of affairs in Washington in which cooperation shall be the keynote of the government's dealings with aeronautical construction. The meeting was called to give the government officials a chance to say definitely and concisely what they want and to give the manufacturers a chance to explain the difficulties and problems which they have met in dealings with the government authorities.

The chief difficulties with motors complained of by the Army and Navy officers were of four kinds, the first really comprising all the others. The officials complained (1) of lack of reliability, (2) of faulty magnets mounting (3) of defective electric wiring, (4) of inability to get deliveries of the sort of motors they want.

Nearly every manufacturer represented complained of the lack of standardization, the lack of orders. This fault can easily be overcome now that Congress has appropriated more than \$16,000,000 for Army and Navy aeroplanes. The magnificently appropriations of past years have decreased and held up the industry to an extent which it would be almost impossible to estimate.

The magnets mounting problem and the electric wiring problem ought not to be difficult of solution.

The object of pointing these extracts in tabulated form in a reserve conference is to make all the information brought out at the session available to airplane buyers and construction shops.

Secretary of War is authorized to lay to other related ones of the United States Corps, Aviation Section, Signal Corps, to arrive service for purposes of instruction or training for periods not to exceed 15 days per year, provided such will be in excess of such related ones and within the limits of funds available for such purposes and such periods of service may be extended for such number of related ones as may be deemed necessary. Extended time will require the pay and allowances of their respective grades in the Regular Army, and when attendance beyond the limits of the 15 days is required for actual travel from their homes to the place to which sent and return to their homes.

Table of pay of the enlisted force of the Aviation Section, Signal Corps, United States Army, are as follows:

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	15750 to 15800	15750 to 15800
	15800 to 15850	158

The side wing was accomplished by means of a lift framework carrying planes at each end, the steering at afloat was first by deep leading weights, later by steering weights. At the forward end, however, an air slip rubber was placed at the forward end, the side handling of the ship under all conditions was thereby made doubly certain. Before the first and second as well as before the third and fourth sections along the length of the ship, were being rapidly



Fig. 3. Steel Works of the Empire in Berlin, Germany.

around positions, each containing a 357 horsepower Daimler motor. By means of double head pulleys of cast aluminum and steel shafting and pulleys, each motor drove two right and two left turning propellers which were situated at the height of the center of resistance. The machinery installation had a combined weight of 1,470 kilograms, or 32 kilograms per horsepower.

This first ship, with all its faults, furnished a good basis for the development of the rigid system, but greater lifting capacity had to be obtained. No lighter gas could be used, and a decrease in the weight of the material of construction was also impossible. On the contrary, the weight of the gas itself was found to be materially increasing so that it was raised from 138 grams per square meter to 200 grams per square meter, until the proper method of handling the



Fig. 4. Boon of the Empire in Berlin, Germany.

gas itself was found, when the weight was again reduced to 170 grams per square meter. The impossibility was practically accomplished. The weight of the water skin was also raised, as in the first ship the skin used on the earlier motor was found to be too weak and liable to stretch, and had to be replaced by cotton.

To increase the carrying capacity, therefore, there remained nearly the possibility of increasing the size of the gas space within the limits of the hull and the size of the building ship, and a more economical use of aluminum. The introduction of sparsular longitudinal girders in the place of the flat girders, as well as a more efficient application of the gas itself, and the use of a considerable saving in the weight of material used.

The greatest benefit was from the increased lifting capacity

which was brought by this means, was the possibility of a further increase in speed, by the employment of larger motors. Progress in the direction of greater speed was also due to the introduction of more reliable and lighter motors. The increase carrying capacity also gave the possibility of using a thin tank for various applications, being applied, facilities leading to the platform on the upper part of the body of the ship.

A comparison between the "Business" and the first "Empire" hull shows the improvements that have been accomplished in the design in the intervening fourteen years. The diameter has increased from 15.2 to 24.0 meters, the length



Fig. 5. The first Empire of 1920 and the "Business" of 1934.

from 136 to 340 meters, whereas the length in only one inch the diameter as opposed to thirty inches. The diameter in the original ship, the contacts from 11,500 cubic meters to 20,000 cubic meters, an increase of 9,500 cubic meters, which means an increase in lifting force of 1,000 to 15,000 kilograms.

The altered polygon has been changed to 37 meters, and the former line motor has been lengthened to 28 meters which is after point is now 32 meters long. The "Business" has 11 compartments. The style of construction and material has remained the same. While increase in strength has been obtained by the new motor system, which is now being a weight of 915 kilograms per meter of length, yet the last which stands out most is that in spite of the relatively smaller lifting capacity obtained with the first ship there was a saving of distance of the frame at about 10 centimeters, while in the latest ship there is an appreciable change in shape, the motor carrying conditions of air.

The first ship developed so many small faults—such as the stretching of the rubber and the failure of the tank, etc., that

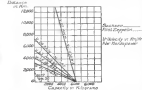


Fig. 6. Capacity of Empire and later types of various powers.

a speed greater than 9 meters per second could not be obtained and it could only carry fuel for about a ten hour trip.

Fig. 5 shows the remarkable increase in power of present ships over the first small ship. The "Business" with a speed of 72 kilometers per hour, a crew weighing 1,000 kilograms, and an available carrying capacity of 3,000 kilograms, makes a record trip of 3,200 kilometers and against a head wind, the weight of the first ship is in glass, and is still able to make a trip of 1,400 kilometers. The more economical the ship is made the first or in other words the ship is made more economical by the decrease in weight. At the speed the length of trip will increase to 2,000 kilometers, with a crew weighing 1,000 kilograms, and an available capacity of 3,000 kilograms.

The Curtiss 250-Horsepower 12-Cylinder Motor

REPORT BY HENRY

The Curtiss Aeroplane Company announces that it has recently built, and is offering for sale to sportmen owners and engine, a twelve cylinder 75" x 57" motor, which was designed for recreational uses primarily. The engine is rated at 250 horsepower but is claimed to develop 300 at 1400 revolutions per minute.

The motor has a cast iron and steel cylinder of the compact type of the motor, the extreme overall length being 80 inches. The cylinder is built into the new form bottom of cylinder (Fig. 1), at the very large, oval-shaped combustion chamber, having a bearing between each crank. The crank pin is of 2 1/2 inches diameter and the main journals of 2 1/2 inches diameter. The bearing caps not only show eight bolts to each end but are also built into the main frame to prevent any lateral movement. Also individual forced lubrication system, through the bottom of each cap where the lead is provided as a bearing. A large cranker three and a half inch diameter.



Fig. 1.

as required in the bearing shown at the left end of the illustration.

In the view looking down upon the motor (Fig. 2) can be seen the two separate twelve-cylinder Daimler motors forming double cylinder, with the consequent reduction of the diameter of the main frame. Two double crankshaft and one. The comparison of this motor, developing as it does 250 horsepower, is well shown here.

The view shown up a pressure pump holding up, for right hand, vertical movement, and also indicates method of mounting the engine. The seven steel tubes giving the support are passed clear through the crankcase, and, therefore, remove all the stress of the mounting. The type which particularly, are just in the right-hand position, is one of two which use the exhaust valves about 1/2 in. at each to relieve compression while working. This also permits gasoline to enter in cylinders when priming through a hole in each exhaust pipe.

By pulling out one of these handles, the motor can be started with no more effort than is required with a regular engine of the same type and stroke or an ordinary portable automobile motor. Installation of self-lubrication is readily possible with this type engine.

GENERAL DESCRIPTION OF CURTISS MOTOR, No. 1.

Type of Motor—12-cylinder water-cooled V-type, separate valves.

At 1400—1400 revolutions per minute normal, 1,500 revolutions per minute maximum, 500 revolutions per minute minimum.

Weight and Stroke—5 1/2 inches.

Weight—Motor, 1,125 pounds; radiator, 130 pounds; cooling water, 120 pounds; propeller, 60 pounds.

Oil Consumption per Horsepower—Four—6 1/2 pints.

Oil Consumption per Hour of Maximum Speed—2 pints.

Distillation Dimensions—Overall length, 80 inches; overall width, 24 inches; overall height, 24 inches; overall depth, 24 inches; height from bed, 30 1/2 inches; depth from bed, 30 1/2 inches.

Weight—Magneto, carburetor, exhaust, manifold, radiator, propeller, lubricator complete, accessories, tools, shipping box.

Ignition—5 high tension 12-cylinder magnets, mounted on front of crankcase cover and driven off timing gear through timing gear shaft. Ignition switch on magnets. Ignition switch on magnets.

Carburetor—4 "bush". Each intake supplies one set of 3 cylinders through 3/4 inch diameter carburetor. This air intake is carburetor through 3/4 inch diameter carburetor. Auxiliary air intake is made up with hand control. Our latest carburetor is 1/2 inch diameter.

Lubrication—Pressure feed. The oil is forced from reservoir in bottom of crankcase by gear pump to one end of hollow crankshaft through crankcase in timing gear and oil pump. Bearings and is carried to main bearings by pressure pipe and through crankcase shown in connecting rod bearings and through crankcase shown in connecting rod bearings. Oil is forced out of the crankcase into the oil pan. Lubrication is not affected by the timing of the motor.



Fig. 2.

Water Circulation—Centrifugal pump fitted to front end of crankcase cover and driven through timing gear mounted on back timing gear.

Cylinders—Made of high carbon steel deep-drawing machined all over. Mount casted side wall turned on. Outside of cylinder heavily ribbed to prevent rust. Cylinders fitted to crankcase by 12 bolts.

Valves—Fitted type in head. Intake shaft steel. Exhaust Tapered steel.

Valve Springs—Coil type intake, offset type exhaust.

Valve Drive—Valve stem direct to cylinder head.

Exhaust Drive—Drive through crankcase and crankshaft.

Cam Followers—Follower type open head steel, crankshaft.

Cam Followers—Follower type open head steel, crankshaft.

Cam Followers—Follower type open head steel, crankshaft.

Cam Followers—Follower type open head steel, crankshaft.

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Cam Followers—Follower type open head steel, crankshaft.

Cam Followers—Follower type open head steel, crankshaft.

By Alexander Klemin, A.C.G.I., R.S.E., S.M.

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PART I—AERODYNAMICS

Effects of Variations in Profile and Plan Form of Wing Sections

As we have seen in Section 5, numerous variations are possible in the profile of wing sections. A slight variation in the profile may, however, introduce considerable changes in the aerodynamic properties of a wing, and necessitate a careful test. Experiments conducted at the various laboratories on variations of number, of position of maximum ordinates, on the thickening of leading and trailing edges, and so forth, have therefore rather a confusion than a systematic appearance. But the results obtained deserve attention, and may serve as a guide to useful modifications. The most important of these experiments are summarized here, and a fuller reference list is appended.

Effect of Variation of Position of Maximum Ordinates in a Wing Section of Plane Lower Surface, and Constant Chord 0.100 for Upper Surface

These experiments of the N. P. L. are surely interesting by reason they indicate where approximately the maximum rate of change of a section should be to give the best possible L/D ratio.

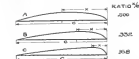


FIG. 1. SECTIONS USED IN INVESTIGATING VARIATIONS OF POSITION OF MAXIMUM ORDINATE

In Fig. 1 are shown a selection of three of the sections tested. They were all developed from one section by altering the position of the maximum ordinate and compensating or expanding the other ordinates to correspond. The lift and drag curves for these sections show considerable variation even in tables as can be seen from the following table:

TABLE 1.

WING SECTION	PLAN SURFACE	MAXIMUM ORDINATE	OTHER SURFACE	CHORD	ANGLE OF INCIDENCE	MAXIMUM ORDINATE	OTHER SURFACE	CHORD
A	0.100	500	0.100	0.100	0.100	500	0.100	0.100
B	0.100	333	0.100	0.100	0.100	333	0.100	0.100
C	0.100	300	0.100	0.100	0.100	300	0.100	0.100

We see that the maximum L/D for section A with a ratio 500 is as high as 13.6, while for section C, where the maximum ordinate is well forward, it sinks to 11. Again, the maximum lift for B is about 50 per cent. greater than that for C. The angle of maximum lift also appears much earlier when the maximum ordinate is nearer the leading edge. A further inspection of the N. P. L. curves also shows that at the point of maximum lift, a slight variation in the ratio changes a smooth bubble point into a dangerously steep one.

The main point of the investigation is to show the case reversed, affecting the position of maximum

*This course commenced in the August 5, 1914 issue of AVIATION and Aerodynamics. Hereinafter, it will be completed in 24 issues. It will contain the design of aeroplanes, and the construction of aeroplanes, and present the design of aeroplanes in general, design, and aerodynamic form.

ordinates for a given section, and also to indicate that the best position is about one third from the leading edge.

Behaviour of Wings with Reverse Curvature at the Trailing Edge

This constitutes a far more important question than that of the preceding paragraph. It would considerably simplify a complete design, from the point of view of stability and lift.



ness of stability if the position of the centre of pressure of the vector of resultant force on the wing did not vary as position is rapidly with change in the angle of incidence. It may be said that as a general rule for the usual angles of flight that when the angle of incidence decreases the centre of pressure on a wing moves far back, and the resultant force is in a line to drive the aircraft back, the wing is unstable. When the angle of incidence increases, the centre of pressure moves forward and the resultant force tends to stall the machine, increasing the angle of incidence still far

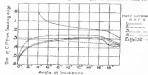


FIG. 3. TRAIL OF CENTRE OF PRESSURE FOR A SERIES OF WINGS WITH UPBENT TRAILING EDGES

then. We shall deal fully with this important point when we consider the general stability of the aeroplane.

Among other means of attaining stability, wings have been designed with a slight reverse curvature at the trailing edge, which have been very successful in keeping the centre of pressure station without further loads. It is important to us to see what sacrifice of efficiency power and efficiency means reverse curvature.

At the N. P. L. a section (No. 1) very similar to that of the H. A. F. 8 was employed, and three reversed curvature forms A, B, C were developed from it by increasing the leading edge, through successively increasing thickness while keeping the

thickness of section unaltered. The point of reference, at which the reducing began, was 15 inch rear 3.4 of the chord from the leading edge, though this could be varied to 3.2 without much effect. Three sections are illustrated in Fig. 2. The point of the centre of pressure is shown in Fig. 3 for all the sections. The curves for the N. P. L. sections show that as the thickness of the leading edge increases, the centre of pressure station becomes further back, and the wing moves toward the leading edge. This is certainly satisfactory from the stability point of view, but the question of efficiency and maximum lift have also to be considered. The following are the values obtained for maximum lift and maximum E_p .

TABLE 2					
SECTION	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT
A	1.00	1.00	1.00	1.00	1.00
B	1.00	1.00	1.00	1.00	1.00
C	1.00	1.00	1.00	1.00	1.00
D	1.00	1.00	1.00	1.00	1.00
E	1.00	1.00	1.00	1.00	1.00

It can be seen that as the rear edge is turned up the L/D and the maximum E_p both decrease proportionally. The main conclusion of the British investigation was that with an increase at the rear edge of about 10% of the chord, the centre of pressure can be kept stationary, but with a loss of 10% per cent. of the maximum L/D and 25 per cent. loss of the maximum E_p . This is a very serious loss, and a sacrifice of the centre of stability and the designer would find other methods of stabilization such as the use of deflexion in biplanes and active stabilizers far more profitable.

Still less, however, investigated a section with a very slight reversed trailing edge (Huff No. 12 Lower-Lower), details of which have been given in Section 31, which is a far more satisfactory and is wide use. Its maximum L/D about 10.2, maximum lift coefficient is about 0.65, and it has an excellent working range. The centre of pressure action is almost and between 5 degrees and 10 degrees of incidence, and with a wing would naturally not tend to drive a machine, although it is not very good at stalling angles. Its shape offers serious constructional difficulties in the region of the rear spar.

Effect of Thickening the Leading Edge of a Wing

Contrary to a somewhat common conception, the thickening of the leading edge as shown in Fig. 4 was distinctly disadvantageous.



FIG. 4. SECTIONS EMPLOYED IN INVESTIGATING EFFECTS OF THICKENING LEADING EDGES

As the angle of incidence increases, the lift coefficient decreases, the decrease in efficiency progressing proportionately to the thickening.

Effects of Thickening Wing Towards the Trailing Edge

Thickening towards the trailing edge is sometimes advantageous from the point of view of structural strength, and experiments have been conducted to see the loss in aerodynamic efficiency such thickening entailed. The sections employed are shown in Fig. 5. It appears from these experiments

EFFECTS OF THICKENING THE TRAILING EDGE OF WING

that the lift coefficient at a given angle of incidence is not much affected at angles below about 5 degrees, but that at smaller angles of incidence the lift coefficient is actually a little greater for the thickened sections. The maximum lift being steadily diminished as the trailing edge is thickened.

TABLE 3					
SECTION	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT
A	1.00	1.00	1.00	1.00	1.00
B	1.00	1.00	1.00	1.00	1.00
C	1.00	1.00	1.00	1.00	1.00
D	1.00	1.00	1.00	1.00	1.00
E	1.00	1.00	1.00	1.00	1.00

As shown in Fig. 6, the section H. A. F. 4 was modified into the H. A. F. 5 to give the well-known "Phillips Entry." This modification was found to have no effect on the aerodynamic properties of the wing, an important consideration in view of

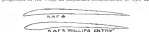


FIG. 6. MODIFICATION OF H. A. F. 4 WING TO GIVE PHILLIPS ENTRY

the fact that numerous attempts have been made to stifle this modification.

Effects of Varying Aspect Ratio

Pope's and Eiffel's experiments have dealt with cambered plates, the N. P. L. has investigated the effect of varying aspect ratio on a pointed wing section rectangular in plan similar to the H.A.F. 10 which is shown in Fig. 7. For



FIG. 7. WING SECTION EMPLOYED AT THE N. P. L. IN INVESTIGATION OF EFFECTS OF VARYING ASPECT RATIO

a more or less accurate understanding of the phenomena accompanying such variation it is necessary to understand the distribution, but for design it is more important to know the simple results of these investigations:

As aspect ratio increases

- (1) The maximum L/D ratio increases, the corresponding angle of incidence increasing steadily the same, and the L/D at other angles improves also.
- (2) The drag diminishes.
- (3) The lift coefficient at all angles very small angles and the maximum lift coefficient remains practically constant, the maximum lift coefficient occurs at a smaller angle of incidence.
- (4) The angle of no lift occurs at smaller positive angles, or larger negative angles as the case may be.

Although the H.A.F. wing tested by the N. P. L. was of pointed form, it is not commonly employed in modern construction. The correction tables (Tables 4 and 5) are based on results derived from it, and it does not at all follow that similar corrections would apply to wings of other forms. In detail of other experimental work, however, such corrections can be applied with probably a few degrees of accuracy. The values for aspect ratio of 6 are taken as a standard of comparison, this being the aspect ratio used for so much aerodynamical work on wing sections.

TABLE 4. CORRECTIONS TO BE MADE IN L/D WITH VARIATION OF ASPECT RATIO

ASPECT RATIO	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT
6	1.00	1.00	1.00	1.00	1.00
5	1.00	1.00	1.00	1.00	1.00
4	1.00	1.00	1.00	1.00	1.00
3	1.00	1.00	1.00	1.00	1.00
2	1.00	1.00	1.00	1.00	1.00
1	1.00	1.00	1.00	1.00	1.00

The following table shows the ratio of drag to lift for aspect ratio 6 as unity.

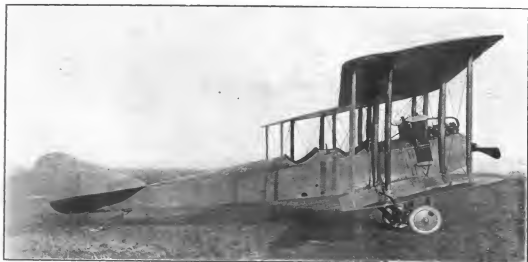
TABLE 5. CORRECTIONS TO BE MADE IN D WITH VARIATION OF ASPECT RATIO

ASPECT RATIO	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT	MAXIMUM E_p	MAXIMUM LIFT
6	1.00	1.00	1.00	1.00	1.00
5	1.00	1.00	1.00	1.00	1.00
4	1.00	1.00	1.00	1.00	1.00
3	1.00	1.00	1.00	1.00	1.00
2	1.00	1.00	1.00	1.00	1.00
1	1.00	1.00	1.00	1.00	1.00

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